

Using ANSYS® Based Aluminum Reduction Cell Energy Balance Models to Assist Efforts to Increase Luralco's Smelter Productivity

Marc Dupuis

GENISIM

Claude
Fradet



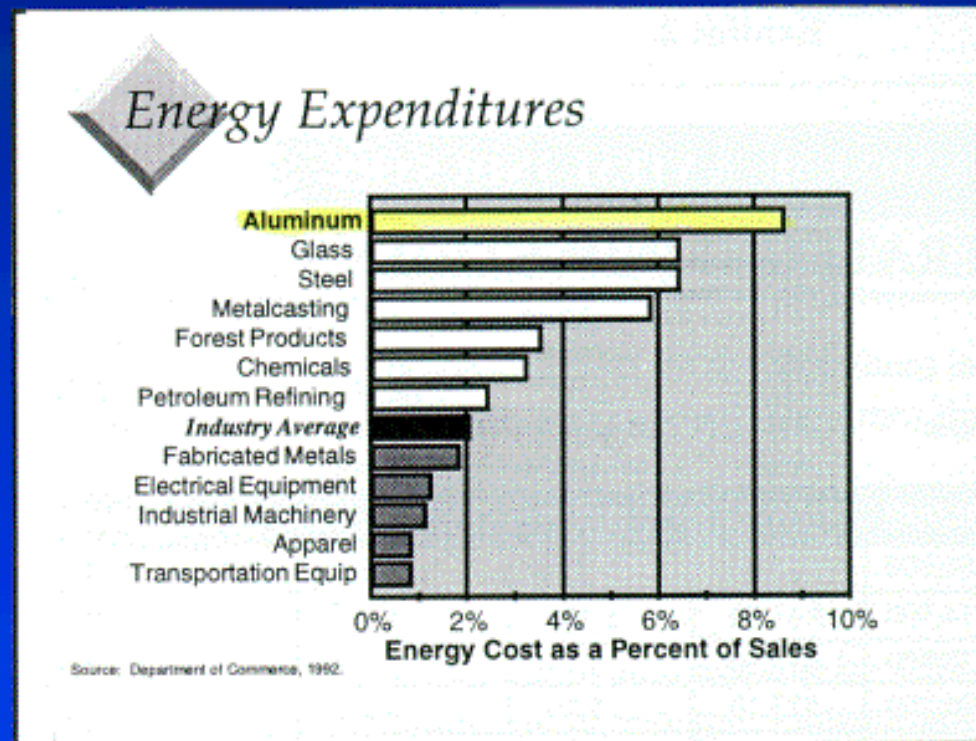
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Plan of the Presentation

- Introduction
- The Hall-Héroult Cell
- Modeling the Hall-Héroult Cell
- Thermo-electric Half Anode Model
- Thermo-electric Cathode Slice Model
- Thermo-electric Quarter Cathode Model
- Validation of the Model Results
 - Thermal Blitz
 - Instrumented Cathode Lining
 - Instrumented Anode
- Initial Smelter's Productivity Improvement
- Conclusions

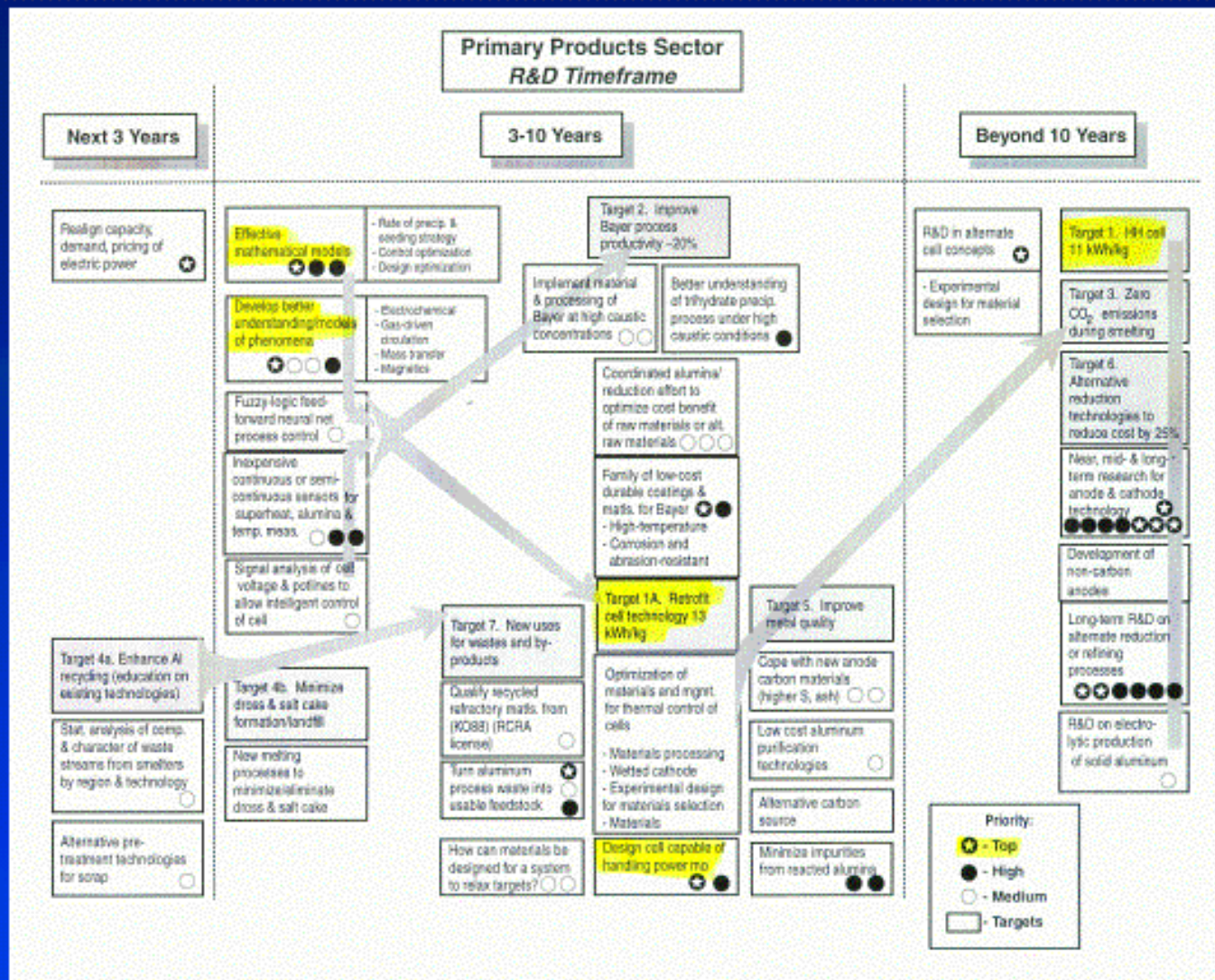
Introduction

Aluminum Production is One of the Most Energy Extensive Industrial Process



Introduction

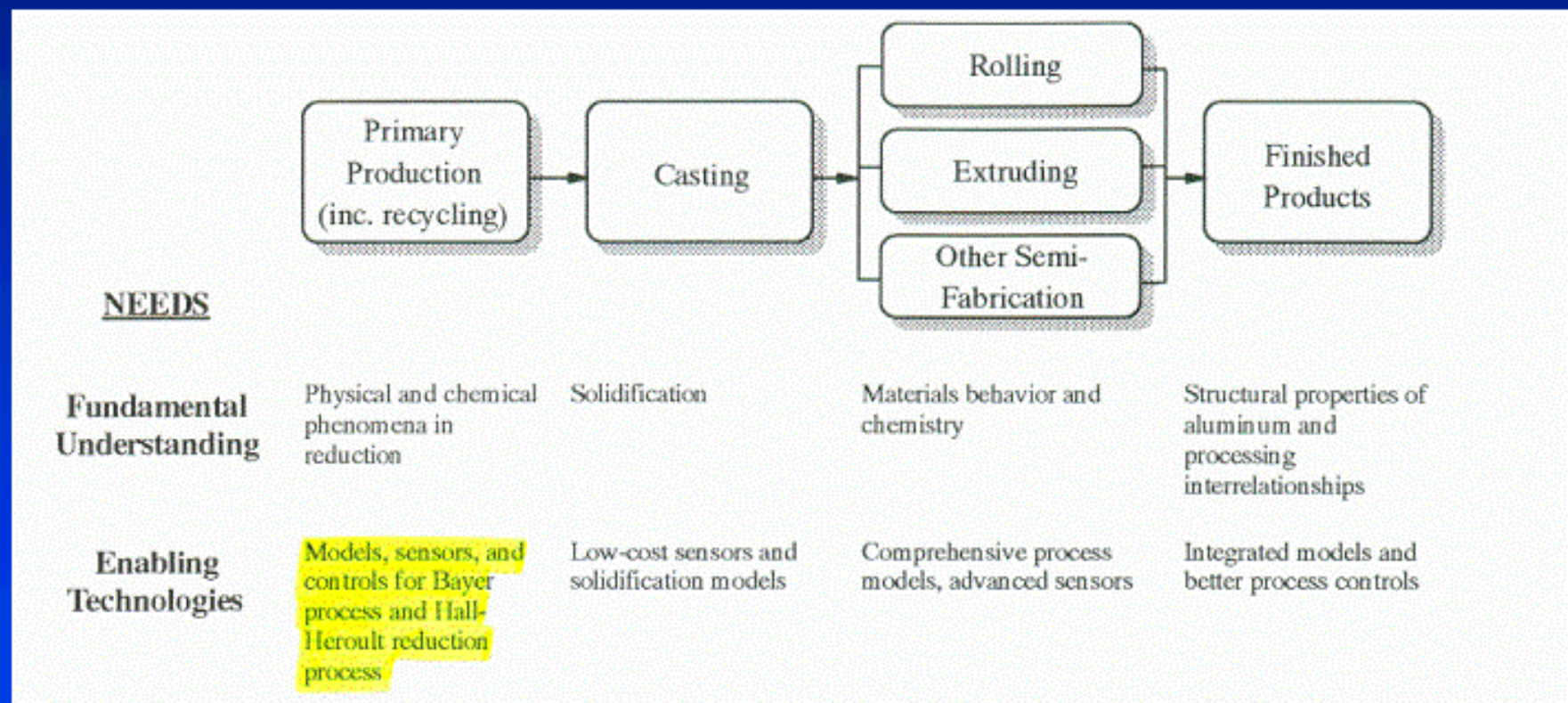
US Department of Energy's Technology Road Map to Reduce the Industry Energy Consumption



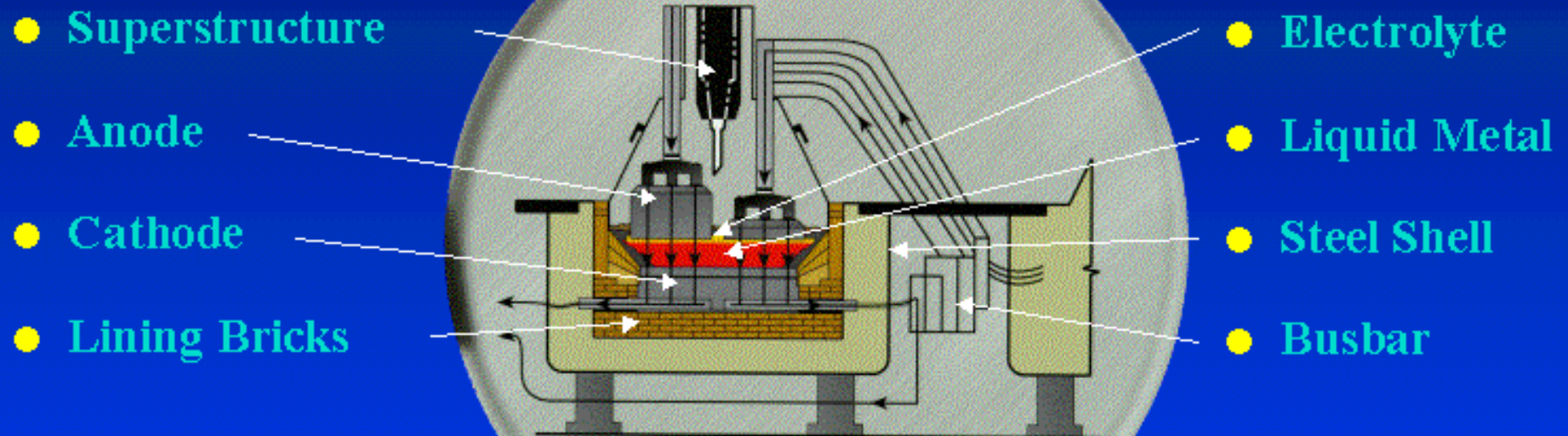
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Introduction

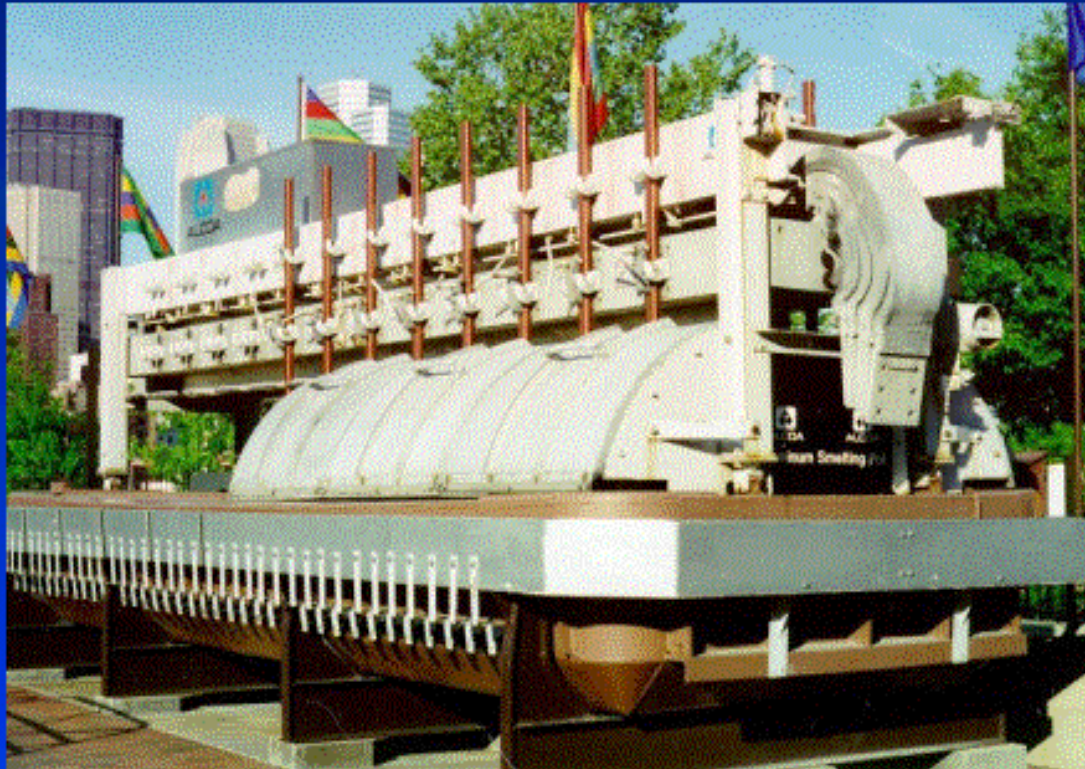
“Effective Mathematical Models” Identified as One of the Key “Enabling Technologies”



The Hall-Héroult Cell



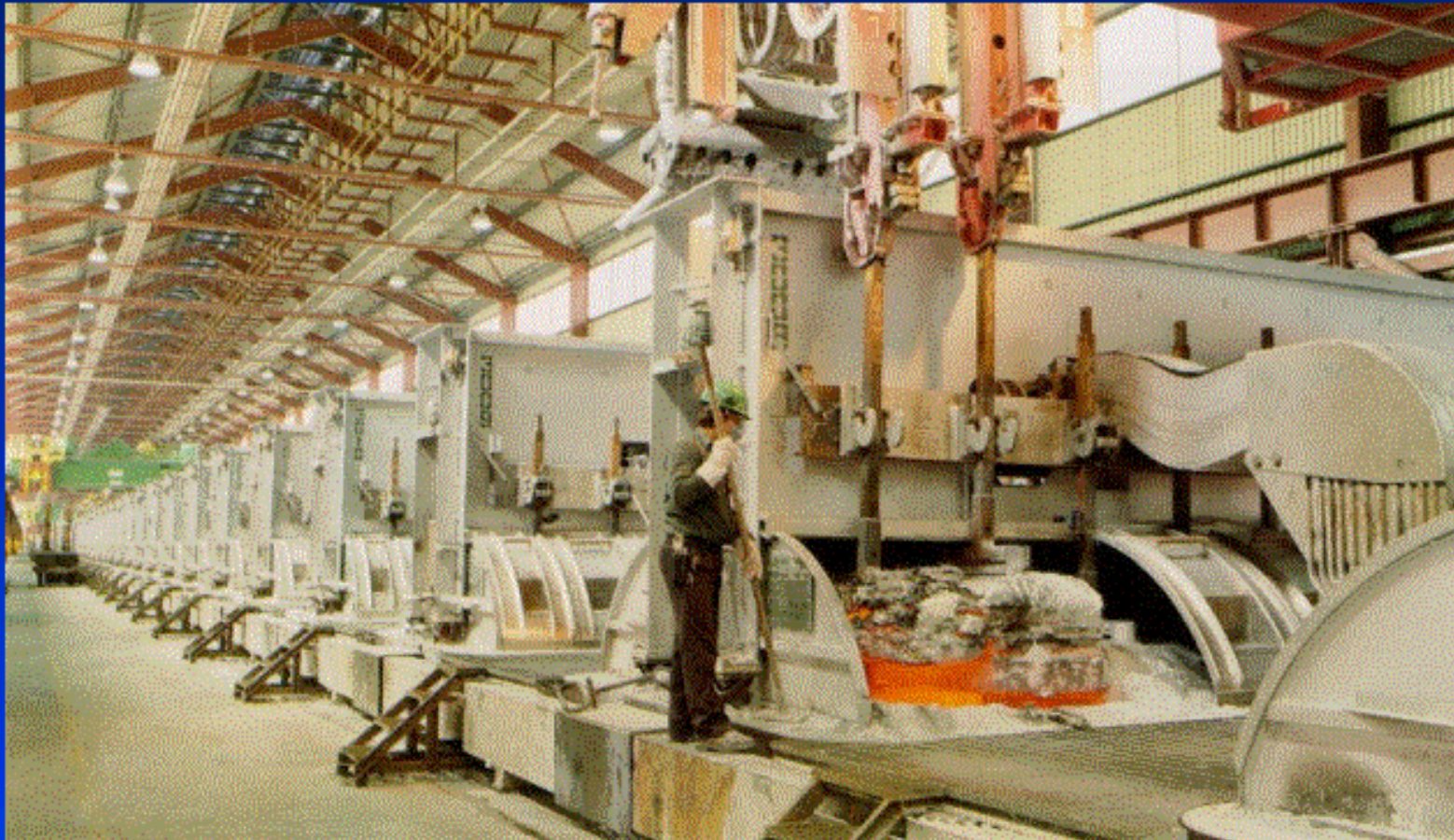
The Hall-Hérault Cell



Pictures from Across the River

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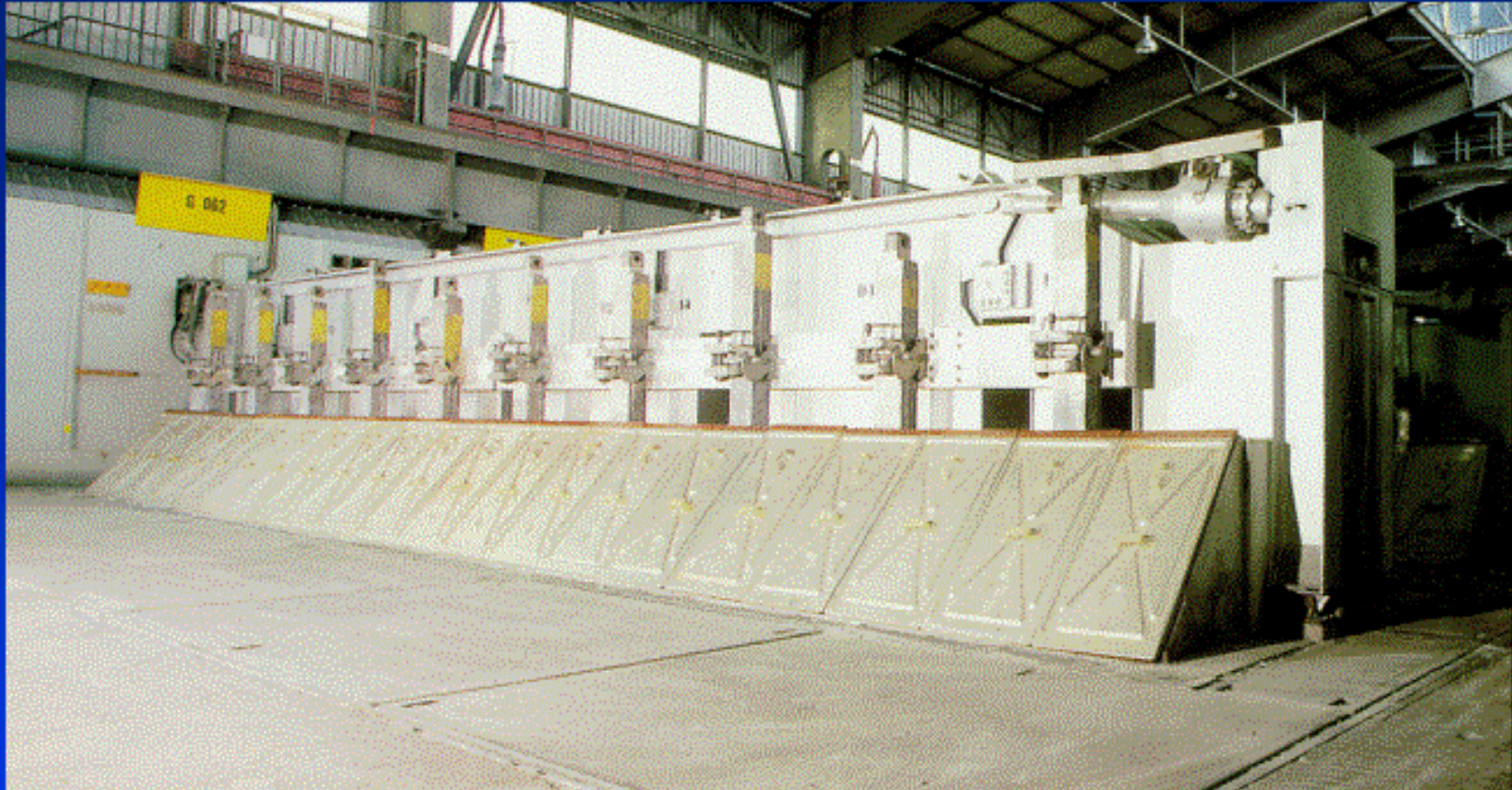
The Hall-Héroult Cell



One of the Last American Design Smelter Built

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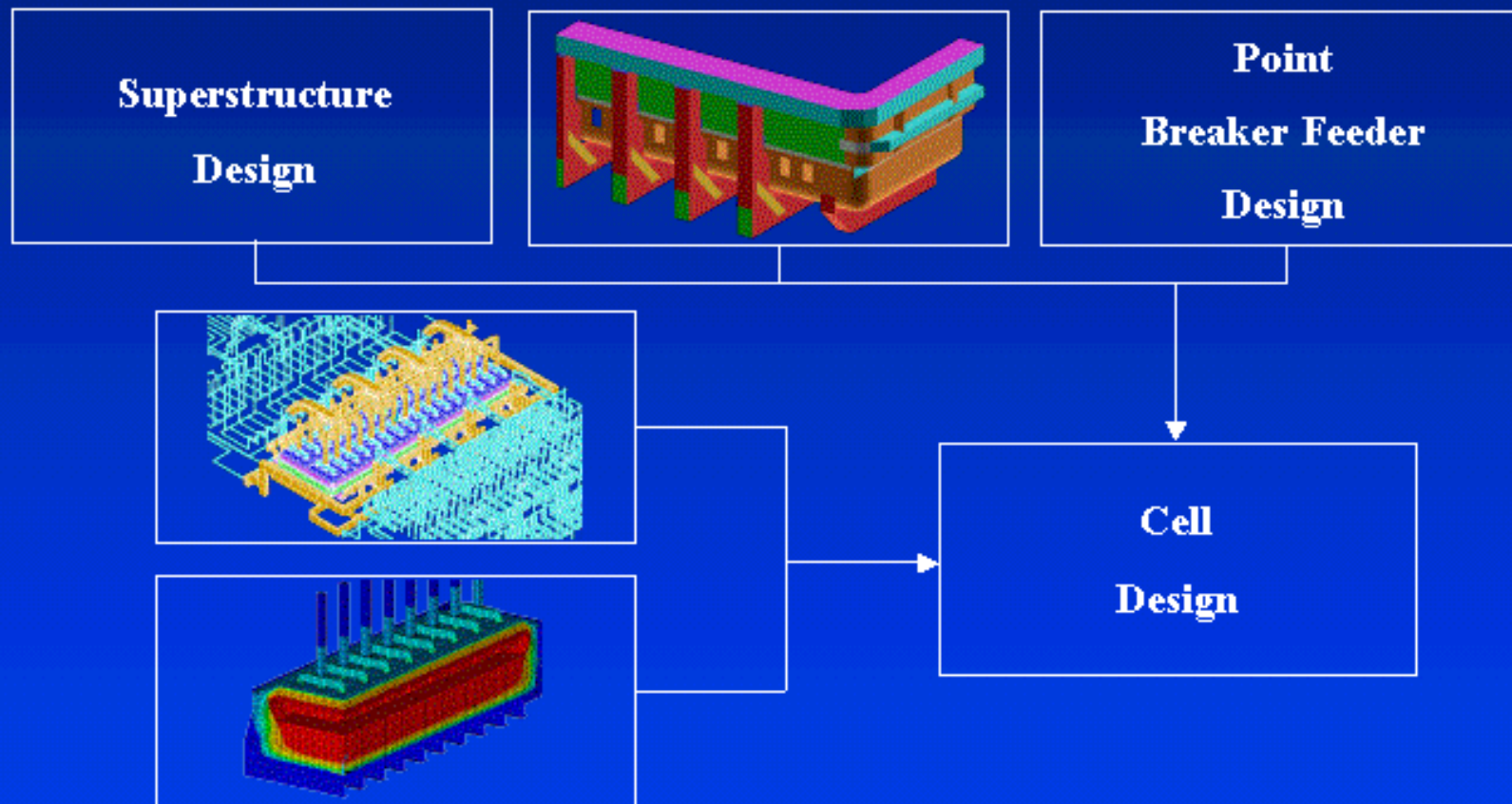
The Hall-Hérault Cell



The Most Modern Technology:
The AP30 from Pechiney France

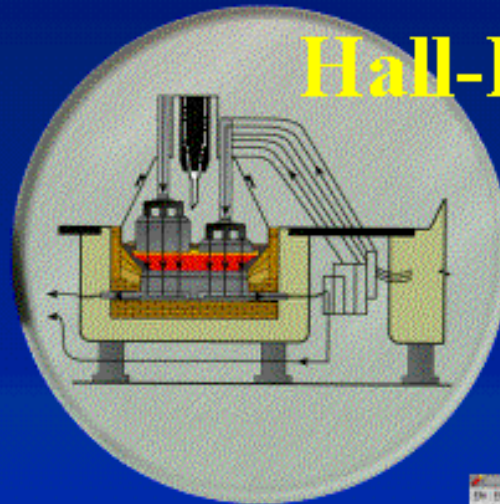
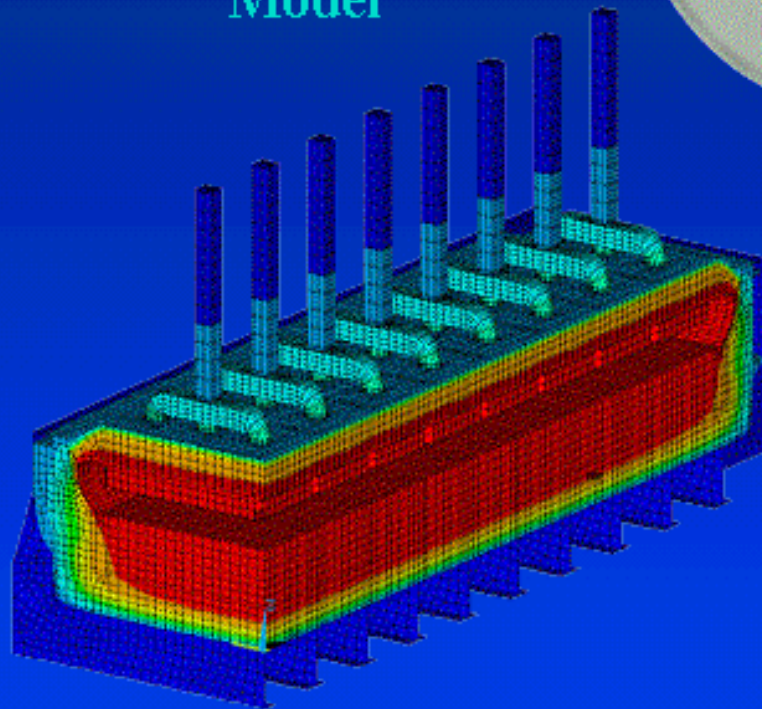
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Modeling the Hall-Hérault Cell



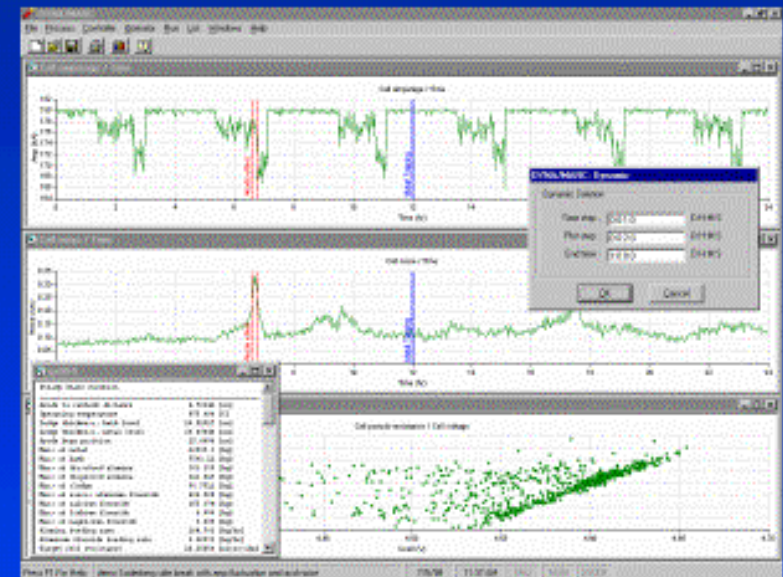
Modeling the

Thermo-electric
3D Steady State
Model



Hall-Héroult Cell

Thermo-electric
1D Dynamic Model



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Thermo-electric Half Anode Model

HEAT BALANCE TABLE			
Half Anode Model 1 : "VAM" 311			

HEAT INPUT	W	W/m^2	2

Bath to anode carbon	1581.54	1538.68	42.86
Bath to crust	611.64	3384.88	18.81
Joule Heat	1396.94		59.15

Total Heat Input	3589.13		188.81

HEAT LOST	W	W/m^2	2

Crust to air	1433.63	1691.43	39.15
Studs to air	1819.63	4168.84	49.69
Aluminum rod to air	488.58	693.18	11.16

Total Heat Lost	3651.16		188.81

Solution Error	2.58	2	

ANODE PANEL HEAT LOST	W	W/m^2	2

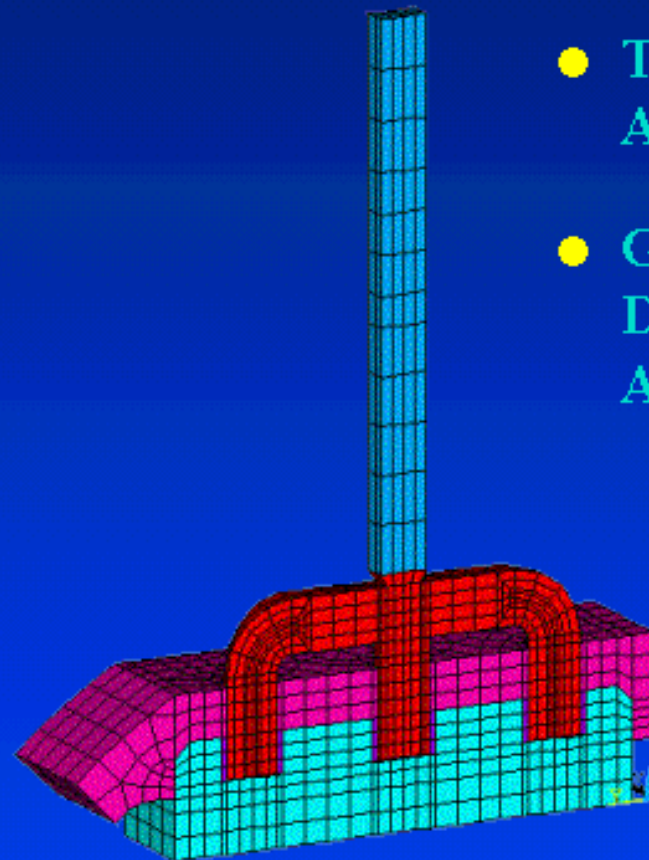
Crust to air	91.15	1691.43	39.15
Studs to air	116.46	4168.84	49.69
Aluminum rod to air	26.14	693.18	11.16

Total Anode Panel Heat Lost	234.55		188.81

	Avg. Drop at clamp [mV]	Current at anode Surf [Amps]	

	582.185	4681.588	

Targeted cell current: 51888.88 Amps			
Obtained cell current: 51888.88 Amps			
Solution Error 1.88 2			



- Total Voltage Drop Across the Anode
- Global Heat Dissipation Across the Anode Panel

Thermo-electric Cathode Side Slice Model

- Total Voltage Drop Across the Cathode Lining
- Global Heat Dissipation Across the Cathode Lining

**** HEAT BALANCE TABLE **** **** Side Slice Model : "VAX" 311 **** **** Freeze profile converged **** **** after 7. iterations ****			

HEAT INPUT	W	W/m^2	t

Bath to Freeze	765.88	8888.88	17.24
Metal to Freeze	1471.68	14588.86	33.13
Metal to carbon	1882.48	1687.15	22.57
Double heat	1281.75		27.85

Total heat input	4401.81		100.85

HEAT SORT	W	W/m^2	t

Shell wall above bath level	641.76	1284.88	14.38
Shell wall opposite to bath	412.86	5161.22	8.26
Shell wall opposite to metal	422.58	7328.48	8.48
Shell wall opposite to block	885.81	5722.22	18.84
Shell wall below block	84.77	665.54	2.15
Shell floor	333.18	414.82	7.47
Cradle above bath level	26.21	1514.37	8.58
Cradle opposite to bath	181.83	2875.57	2.27
Cradle opposite to metal	66.45	2546.87	1.48
Cradle opposite to block	261.83	828.84	5.87
Cradle opposite to block	43.64	153.86	8.88
Cradle below floor level	282.55	88.23	4.54
Max and flux to air	627.38	2648.48	14.87
End of flux to burbar	348.32	48514.13	7.63

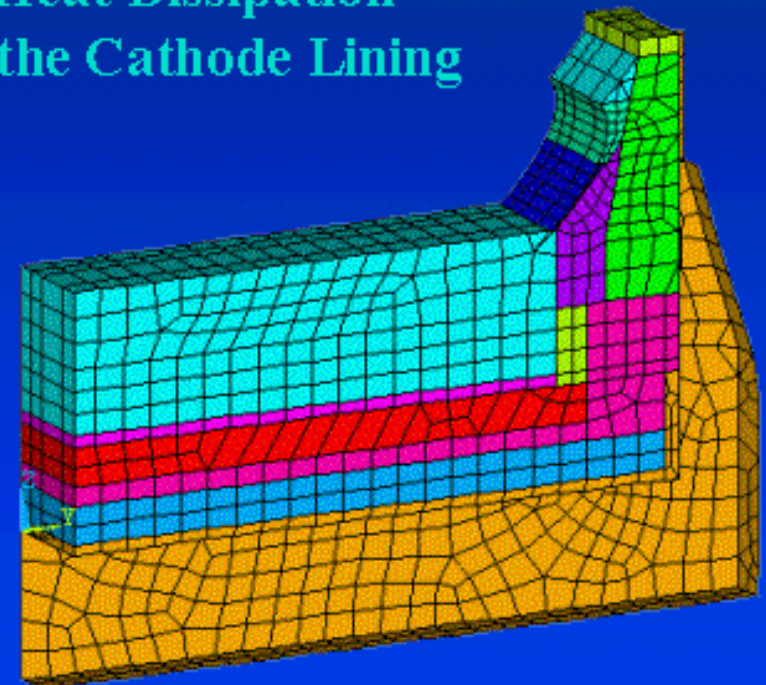
Total heat sort	4458.68		100.85

Solution error	5.48 t		

Total Cathode heat sort	385.32		100.85

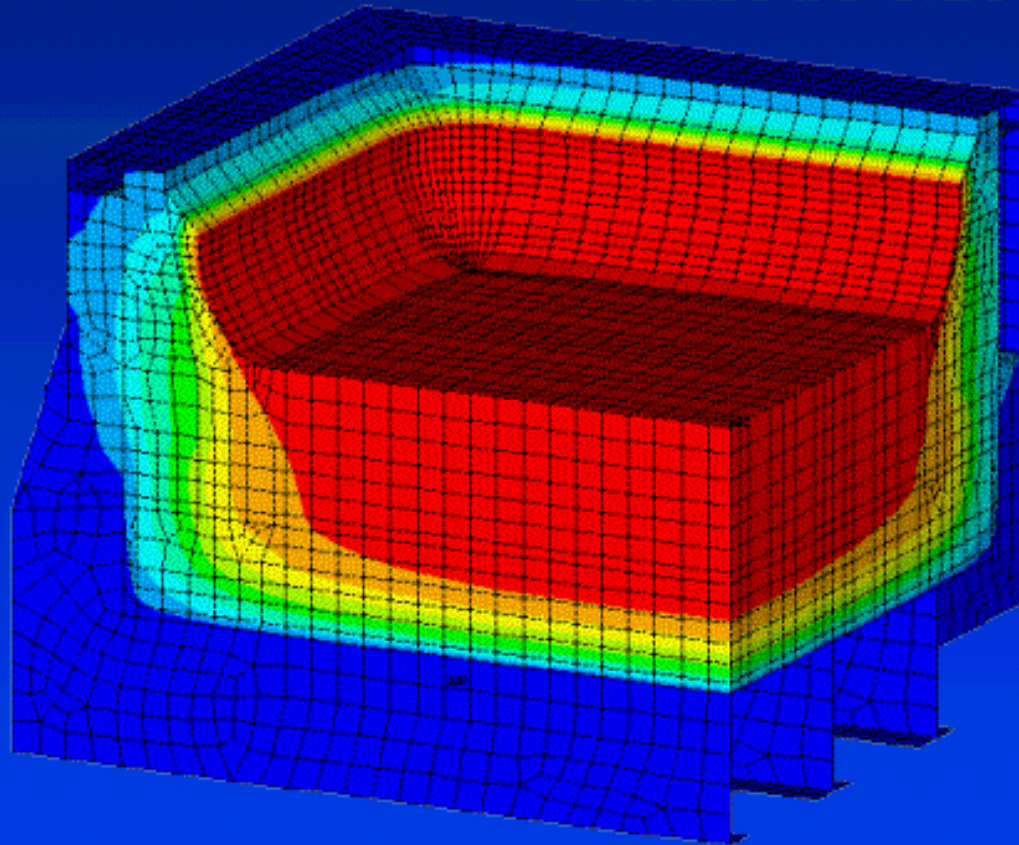
Avg. drop at max end [mv]	Average flux. drop [mv]	Current at Cathode flux [amps]	
-----	-----	-----	
285.268	7.473	4166.667	

targeted cell current:	38888.88 amps		
Obtained cell current:	38888.88 amps		
Solution error	5.88 t		



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Thermo-electric Corner/Quarter Cathode Model



- More Accurate Global Cathode Heat Dissipation
- Total Voltage Drop Across Cathode Lining
- Corner Ledge Profile

Validation of the Model Results



Thermal Blitz: Heat Flux Measurements

Thermal Blitz: Results

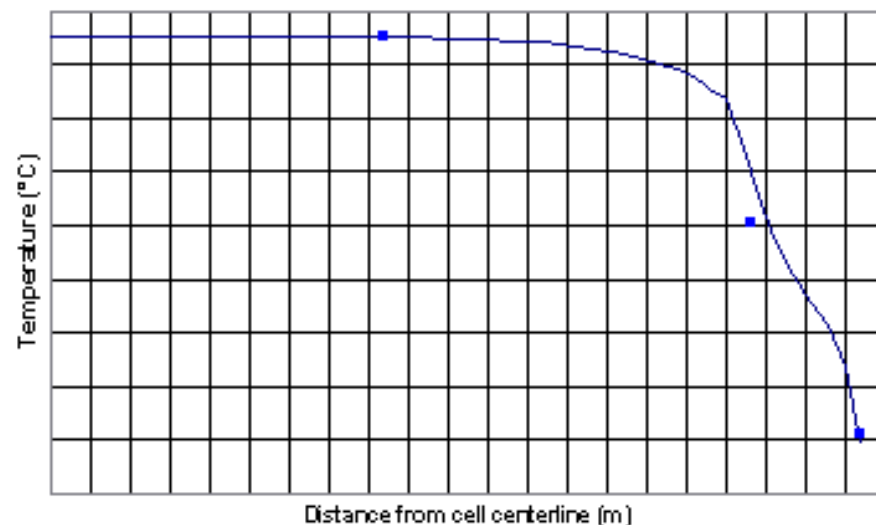
Heat Flux Measurements for Cell Heat Balance		
date:	8-Sep-97	slice no: A2
cell:	"GMP" 300	
Shell Wall		
Description	Flux	Temp
Wall above deck level	2000	130
Wall deck level	5500	230
Wall metal level	7300	230
Wall block level above dsc	6000	235
Wall concrete dsc	5000	190
Right collector dsc	3000	190
Wall concrete dsc level	1300	80
Wall deck level	1000	60
Flange near centerline	300	30
Flange at Quebec point	500	50
Flange near corner	300	30
Cradle web		
Wall above deck level	1000	100
Wall deck level	2165	130
Wall metal level	2880	190
Wall block level above dsc	955	125
Wall concrete dsc level	900	80
Wall deck level	155	50
Flange extension	0	0
In line corner	100	35
Wall extension above section	0	0
Wall extension above section	0	0
Flange near centerline	100	35
Flange at Quebec point	100	35
Flange near corner	100	35
Cradle flange		
Wall above deck level	300	65
Wall deck level	1085	80
Wall metal level	1350	90
Wall block level above dsc	475	40
Wall concrete dsc level	200	35
Wall deck level	50	30
Flange line flange	30	30

Heat Balance Results			
date:	8-Sep-97	Cell:	"GMP" 300
Cathode Heat Losses	W/ m2	kW	%
Shell side wall above back level	1000	11.51	1.86
Shell side wall opposite to back	5500	11.68	5.11
Shell side wall opposite to metal	7500	11.10	6.97
Shell side wall opposite to block above bar	6000	11.18	7.80
Shell side wall opposite to block between bars	1500	6.18	1.05
Collector bars to air	1000	17.18	1.79
Collector bars to flexible		60	9.68
Shell side wall opposite to brick	1000	11.51	1.86
Shell floor close to corner	500	12.51	1.01
Shell floor quarter point region	500	10.11	1.68
Shell floor centerline region	500	8.11	1.11
Cradle above back level	889	6.08	0.98
Cradle opposite to back	1935	11.17	1.13
Cradle opposite to metal	2165	16.17	1.61
Cradle opposite to block above bar	818	8.12	1.11
Cradle opposite to block between bars	156	1.17	0.19
Cradle opposite to brick	111	1.80	0.19
Cradle corner	51	1.51	0.15
Cradle below floor close to corner	100	1.76	0.11
Cradle below floor quarter point region	100	1.76	0.11
Cradle below floor centerline region	100	1.76	0.11
Shell end wall opposite to metal	1500	1.61	0.11
Shell end wall opposite to block above bar	1000	7.11	1.18
Shell end wall opposite to block below cap of bar	1000	6.18	1.11
Shell end wall opposite to brick	1000	10.11	1.68
Shell coverplate in the ends	500	1.51	0.15
Shell horizontal stiffeners in the ends	1181	18.00	1.90
Shell vertical stiffeners in the ends	898	5.51	0.89
Shell horizontal stiffeners in the ends	100	0.15	0.01
Total for the cathode part		371.76	59.95
Anode Heat Losses			
Cross in side channels	1700	11.18	1.16
Cross above anodes	1800	8.19	11.11
Cross in center channel	1750	1.60	0.58
Scum	1000	17.11	1.18
Yoke	1610	8.17	11.51
Aluminum rod	811	10.11	1.89
Total for the anode part		118.3	19.05
Total for the cell		610.1	100.00

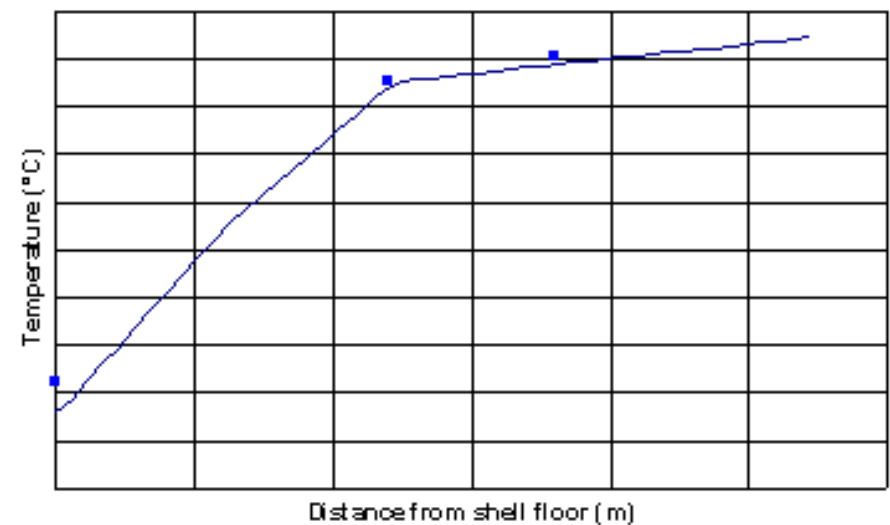
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Validation of the Model Results

Horizontal temperature in lining at BIL/BRO interface



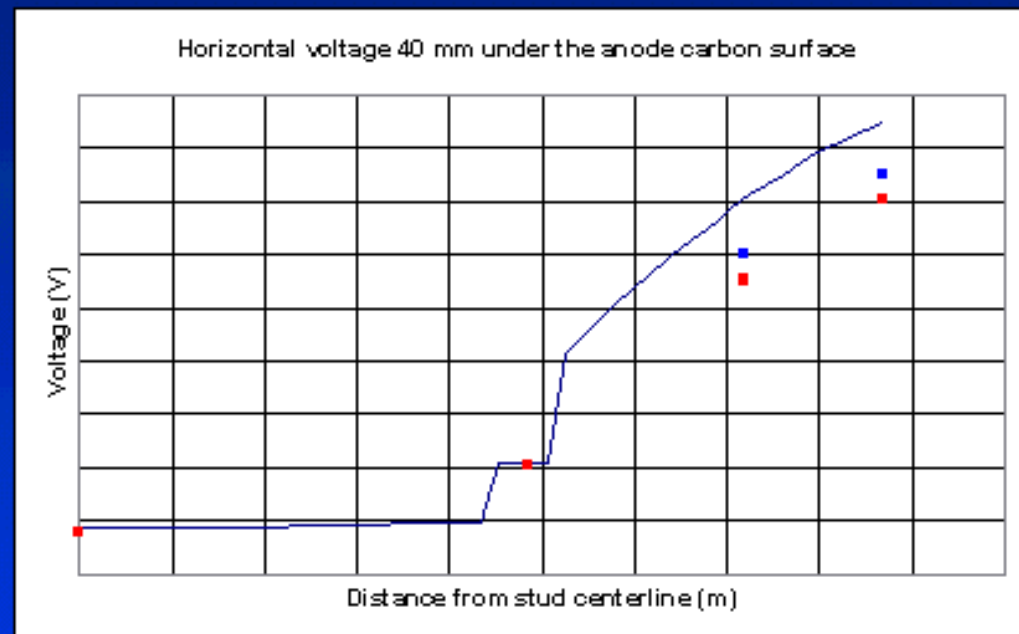
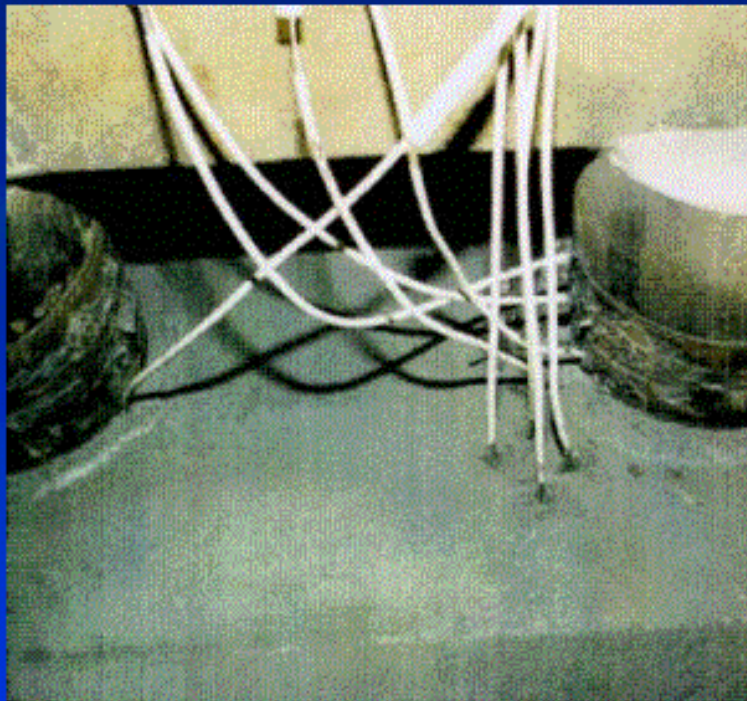
Cell centerline vertical temperature under block



Instrumented Cathode Lining:
Cathode Lining Temperature Comparison

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Validation of the Model Results



**Instrumented Anode:
Anode Stud Voltage Drop Comparison**

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Initial Smelter's Productivity Improvement

		START-UP	LATEST POTS
PRODUCTION :			
▪ Production per pot/day	(kg)	2245	2466
▪ Current efficiency	(%)	94.5	96
POWER :			
▪ Amperage	(kA)	295	319
▪ Pot voltage	(V)	4.330	4.185
▪ DC kWh/t		13 650	13 000
CONSUMPTIONS :			
▪ Gross carbon	(kg/t)	540	493
▪ Net carbon	(kg/t)	410	397
▪ Anodes cycle-shifts-8 hours		80	90
METAL PURITY :			
▪ Iron	(ppm)	---	700
▪ Silicon	(ppm)	---	240
POT CONDITION :			
▪ Anode effects	(pot/day)	0.40	0.20

Tableau no. 1 : Lauralco's results



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Conclusions

- **The Models represent for Luralco Powerful Tools to Pursue the Development of the Technology**
- **The development of the Models was for Luralco a Strong Learning Process**